

Natura Resources
SUSTAINABLE ENERGY

Background

Overview

- | Isotope | σ_a [b] |
|-------------------|----------------|
| U ²³⁵ | 5.1E2 |
| Xe ¹³⁵ | 2.6E6 |
| Sm ¹⁴⁹ | 4.2E4 |

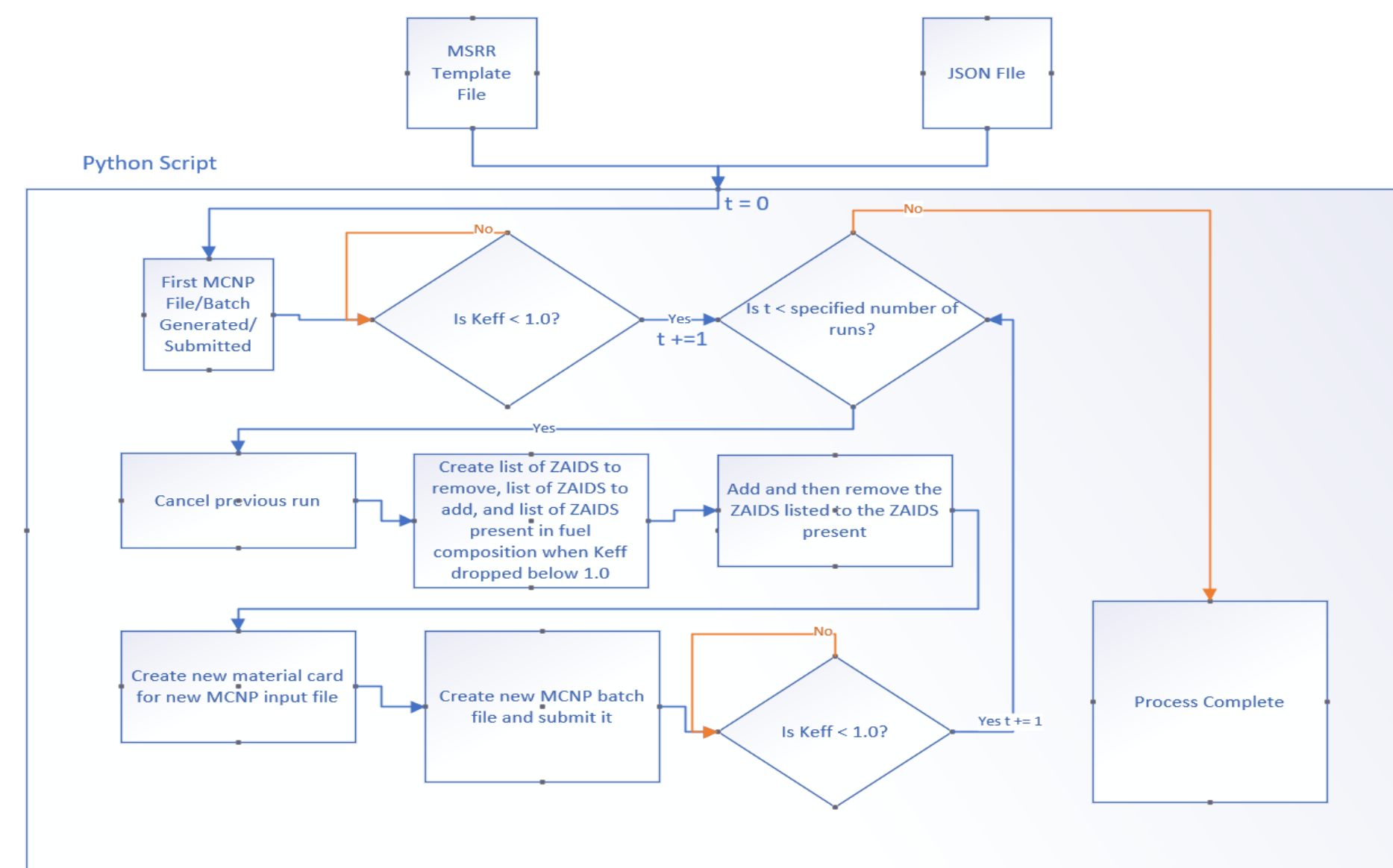
- $$\begin{aligned} \frac{dN_{Xe}}{dt} &= \gamma_{Xe} \Sigma_f \phi + \lambda_I N_I - \lambda_{Xe} N_{Xe} - \sigma_a^{Xe} N_{Xe} \phi - \text{removal rate} + \text{reinsertion rate} \\ \frac{dN_{Sm}}{dt} &= \lambda_{pm} N_{pm} - \sigma_m^S N_{Sm} \phi - \text{removal rate} + \text{reinsertion rate} \end{aligned}$$

Logic

-
- ```

graph LR
 Start([Start Reactive Operation]) --> Continue[Continue Operation
(Depurin Feed)]
 Continue --> Ksp{Has Ksp dropped below the threshold?}
 Ksp -- No --> Continue
 Ksp -- Yes --> Desired{Is continued operation desired?}
 Desired -- Yes --> Refill[Refill and/or
Remove Me3+ and
or Sn4+]
 Refill --> Continue
 Desired -- No --> End([End Reactive Operation])

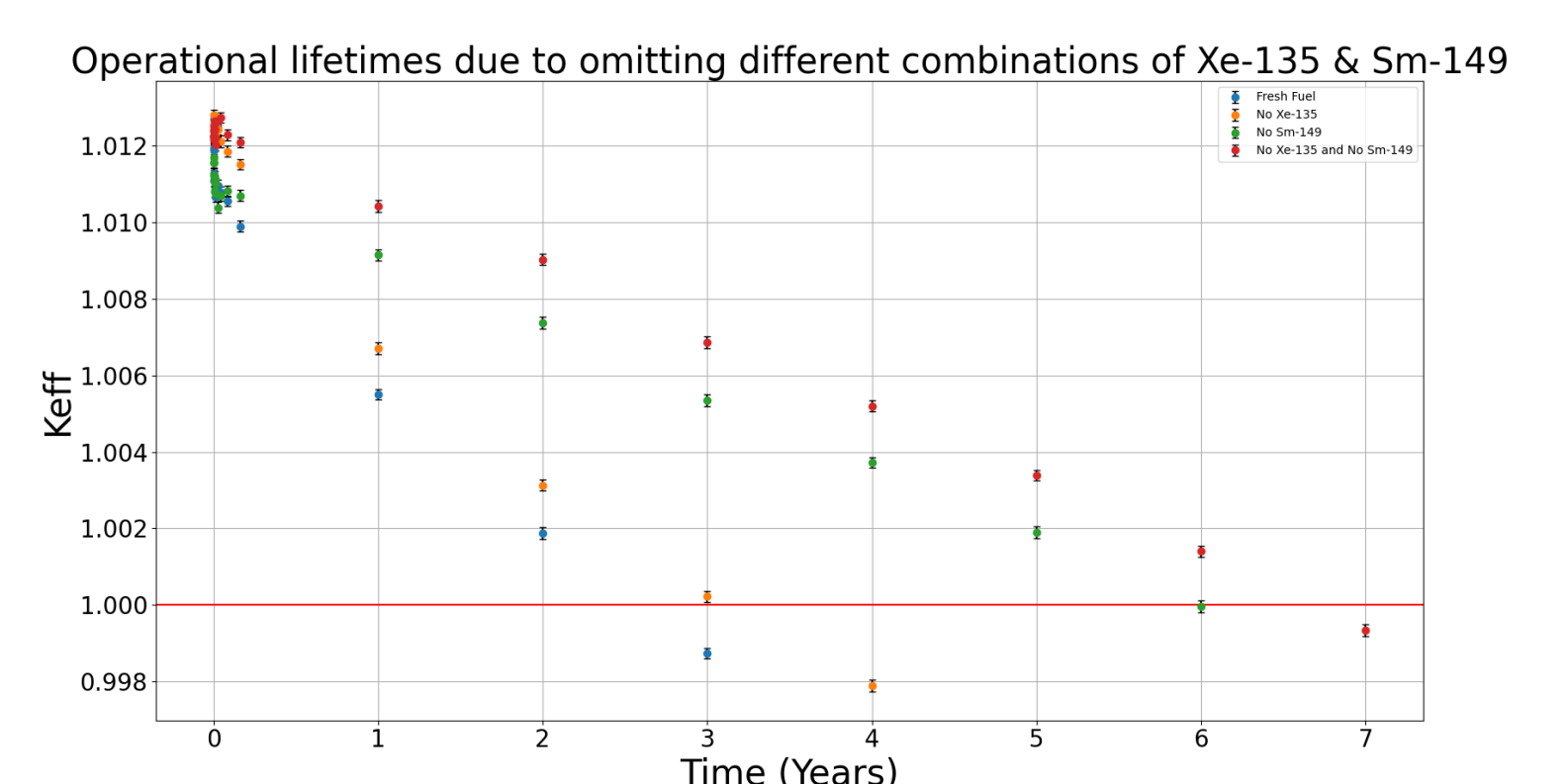
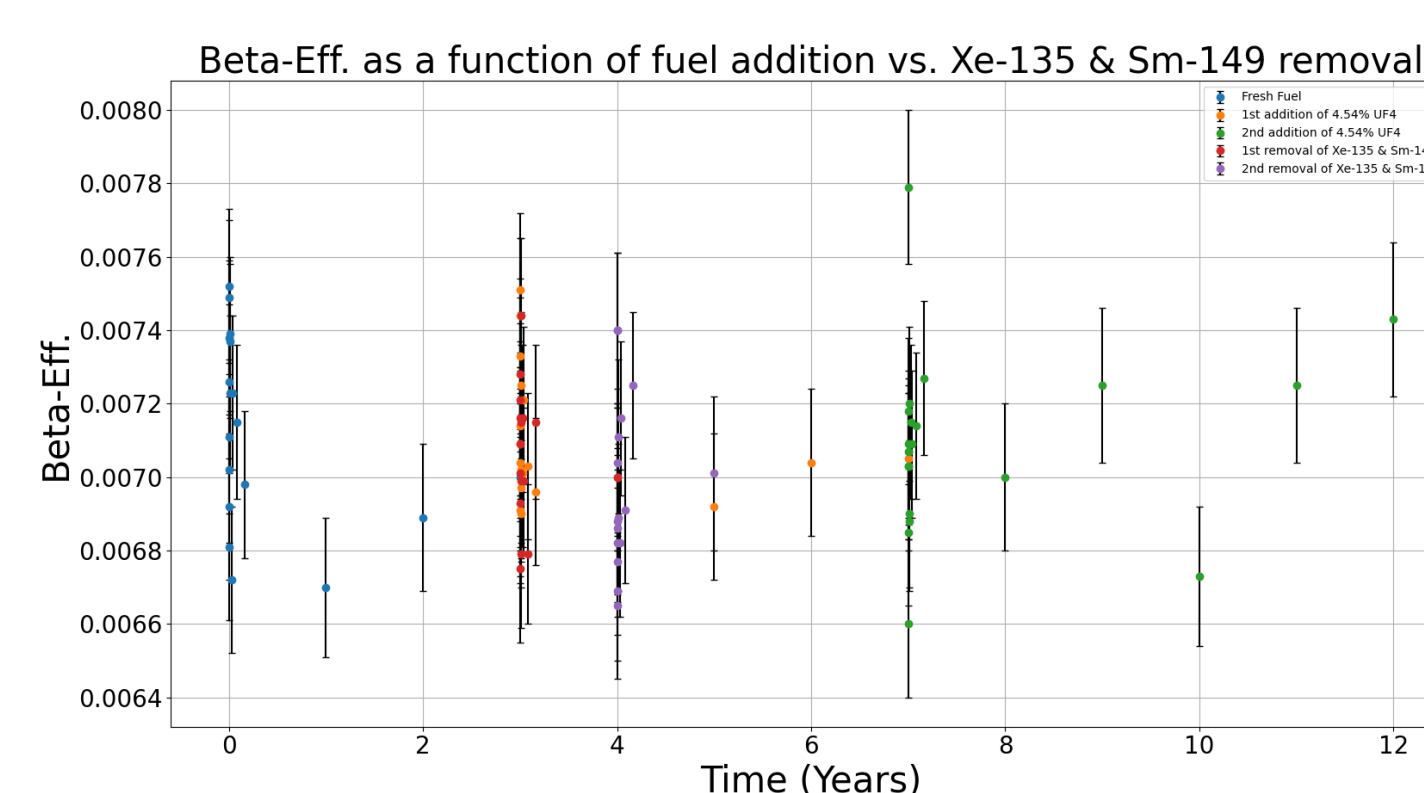
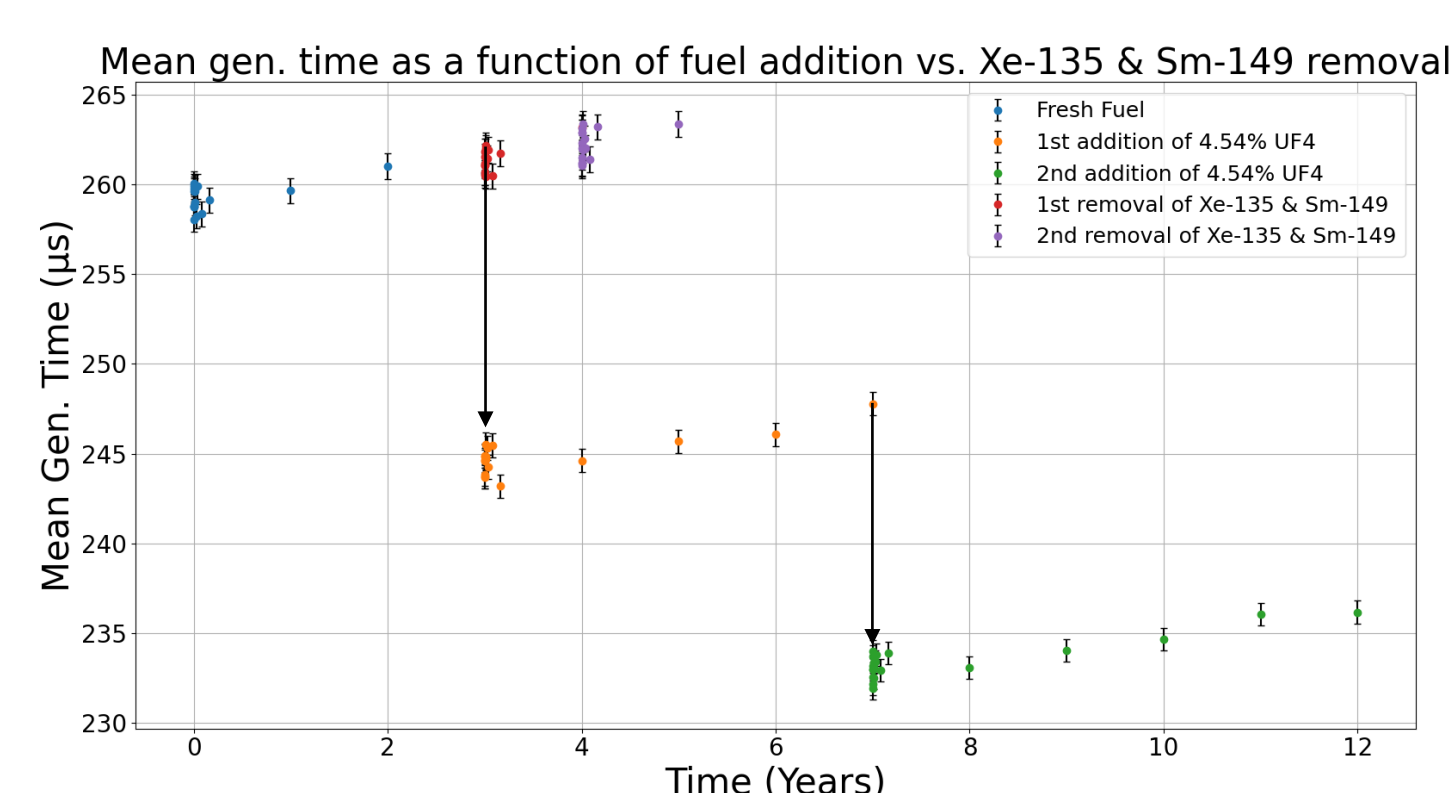
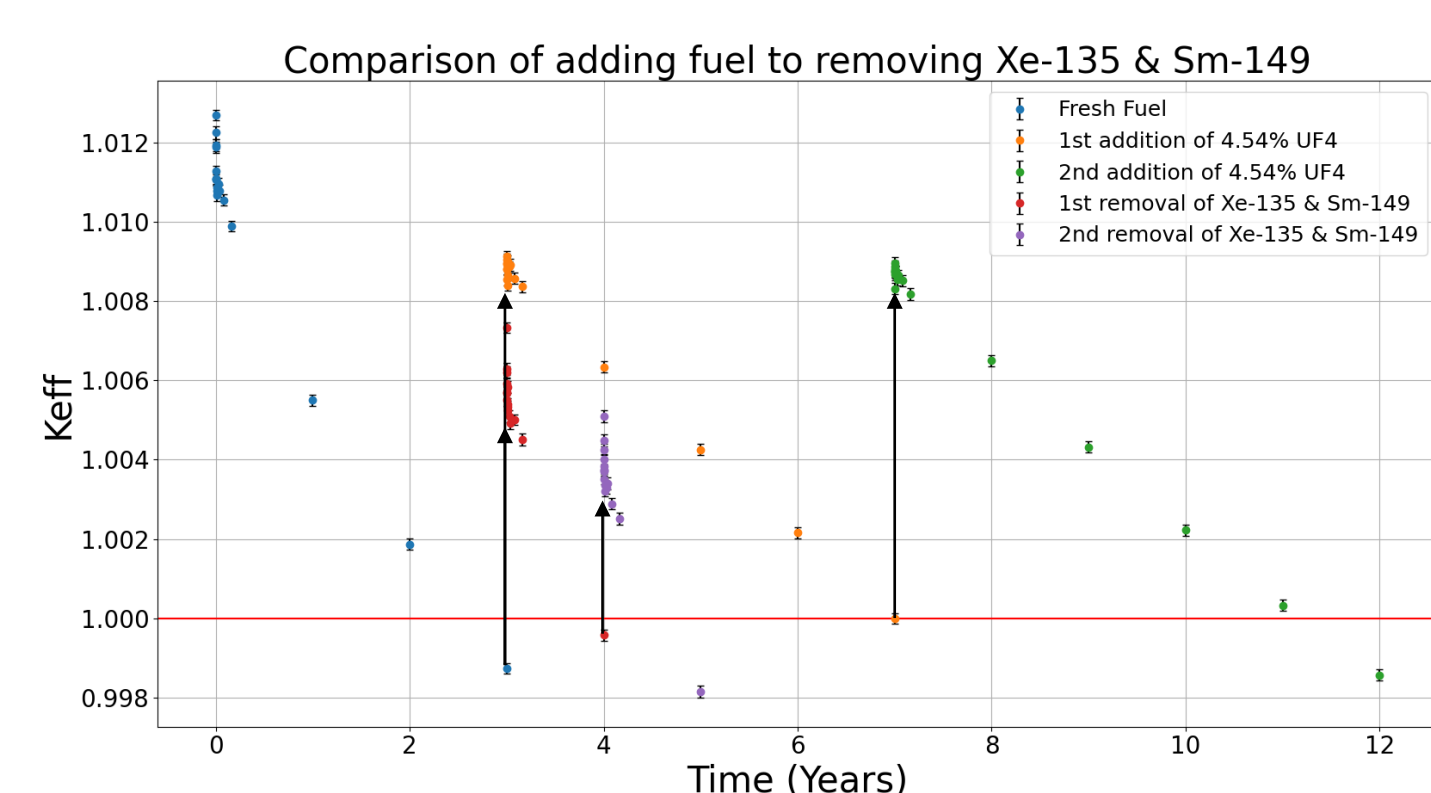
```
- The flowchart illustrates the control strategy for the reactive operation of a power plant. It begins with a 'Start Reactive Operation' terminal, leading to a 'Continue Operation (Depurin Feed)' process. This process leads to a decision diamond: 'Has  $K_{sp}$  dropped below the threshold?'. If the answer is 'No', the flow loops back to the 'Continue Operation' process. If 'Yes', it proceeds to another decision diamond: 'Is continued operation desired?'. If 'Yes', it leads to a process box 'Refill and/or Remove  $Me^{3+}$  and or  $Sn^{4+}$ ', which then loops back to the 'Continue Operation' process. If 'No', it leads to the 'End Reactive Operation' terminal.



| step | duration<br>(days) | time<br>(days) | power<br>(MW) | keff    |
|------|--------------------|----------------|---------------|---------|
| 0    | 0.000E+00          | 0.000E+00      | 1.000E+00     | 1.01270 |
| 1    | 2.500E-01          | 2.500E-01      | 1.000E+00     | 1.01226 |
| 2    | 2.500E-01          | 5.000E-01      | 1.000E+00     | 1.01194 |
| 3    | 2.500E-01          | 7.500E-01      | 1.000E+00     | 1.01189 |
| 4    | 2.500E-01          | 1.000E+00      | 1.000E+00     | 1.01128 |
| 5    | 5.000E-01          | 1.500E+00      | 1.000E+00     | 1.01109 |
| 6    | 5.000E-01          | 2.000E+00      | 1.000E+00     | 1.01107 |
| 7    | 5.000E-01          | 2.500E+00      | 1.000E+00     | 1.01110 |
| 8    | 5.000E-01          | 3.000E+00      | 1.000E+00     | 1.01080 |
| 9    | 1.000E+00          | 4.000E+00      | 1.000E+00     | 1.01068 |
| 10   | 1.000E+00          | 5.000E+00      | 1.000E+00     | 1.01088 |
| 11   | 5.000E+00          | 1.000E+01      | 1.000E+00     | 1.01096 |
| 12   | 5.000E+00          | 1.500E+01      | 1.000E+00     | 1.01079 |
| 13   | 1.500E+01          | 3.000E+01      | 1.000E+00     | 1.01056 |
| 14   | 3.000E+01          | 6.000E+01      | 1.000E+00     | 1.00990 |
| 15   | 3.050E+02          | 3.650E+02      | 1.000E+00     | 1.00550 |
| 16   | 3.650E+02          | 7.300E+02      | 1.000E+00     | 1.00187 |
| 17   | 3.650E+02          | 1.095E+03      | 1.000E+00     | 0.99873 |

- MCNP was chosen to model the depletion of the fuel
    - Produced the  $K_{eff}$ , mean generation time, and effective delayed neutron fraction for each depletion step
    - Fission product tier 2 was selected due to computational time
    - Due to the isotope generator algorithm, each subsequent sequential run required increased time
  - Input Parameters:
    - Number of runs
    - Incremental depletion timesteps (days), power fraction for each timestep, operating power (MW), material to be depleted, depletion options such as fission product tier list, material volume, isotopes to be omitted
    - Number of isotopes to remove, the isotope and its corresponding mass to be added or removed between each run
    - The control rod positions (kept constant)
  - MCNP was used in conjunction with Python in order to automate the simulation behavior of online refueling and online fission product removal
    - First run was fresh fuel to provide a baseline for the operational lifetime
      - Subsequent runs will determine at what frequency and magnitude fuel composition changes should occur
    - Lifetime expectations due to fission product removal will be found through the omission of  $Xe^{135}$  &  $Sm^{149}$
  - Output Parameters:
    - $K_{eff}$
    - Mean generation time
    - Effective delayed neutron fraction
    - “Lifetime” of the reactor
      - When  $K_{eff}$  drops below 1.0, it is determined that timestep is the lifetime of the MSRR

## Results



- As can be seen, there was a prompt increase in  $K_{\text{eff}}$  whenever fuel was added or  $\text{Xe}^{135}$  &  $\text{Sm}^{149}$  was removed
- As can be seen, there was a prompt decrease in mean generation time whenever fuel was added, and only a slight, very short-lived effect when  $\text{Xe}^{135}$  &  $\text{Sm}^{149}$  was removed
- As can be seen, the delayed neutron fraction has a relatively large uncertainty but tends to remain around approximately 0.007
- $\text{Xe}^{135}$  &  $\text{Sm}^{149}$  omission increased the lifetime by  $\approx 170\%$
- $\text{Sm}^{149}$  omission increased the lifetime by  $\approx 140\%$
- $\text{Xe}^{135}$  omission increased the lifetime by  $\approx 25\text{-}30\%$

## Conclusions

- Continuous removal of  $\text{Xe}^{135}$  and  $\text{Sm}^{149}$  can extend the lifetime by approximately 170%
- Mean gen. time is sensitive to fuel insertion while influenced to a lesser degree by removal of  $\text{Xe}^{135}$  &  $\text{Sm}^{149}$
- Negligible effects observed on beta-eff.
- If  $\text{Xe}^{135}$  is the only isotope removed, the effects on all affected parameters are short lived (but noticeable)

## Future Work

- Find reliable percentages for solid fission product removal
- Remove fission products on a much shorter time period (Ex. on the timescale of days)
- Run more particles to see if the uncertainty of beta-effective begins to decrease further
- Evaluate the impact of removing the same mass of fuel-salt as the mass of  $\text{UF}_4$  being added

## Acknowledgments



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